

Development and Cost Estimation for Sizing 5 Kw Palm Kernel Shell Steam Boiler

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ABSTRACT: The aim of this study is to develop and estimate the cost of 5 kW Palm Kernel Shell (PKS) steam boiler. Design drawings were produced and used to fabricate PKS combusting unit. Other components needed for the design were selected based on functionality, durability, cost and local availability. Using the developed furnace, maximum combustion efficiency, steam temperature and pressure were estimated based on primary to secondary air supplied. The results showed that the primary to secondary air setting of (40:60) recorded highest combustion efficiency of 64.5% for a fuel feed rate of 17.3 kg/hr. The boiler's maximum steam temperature, pressure and mass flow rate recorded for 5 kW power rating were 220 °C, 0.38 MPa and 0.023 kg/s respectively. The overall cost for sizing the boiler components is cheap (approximately \$ 1,658.906) in comparison to similar design overseas (\$ 2,223.56) and thus will serve as an alternative source of energy.

KEYWORDS: Cost, Furnace, Palm kernel shell, Power, steam generator

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I INTRODUCTION

Agriculture remains one of the important sectors of the economy in Nigeria. It creates employment for about 70 % of Nigeria's populace and contributes about 40 % to the Gross Domestic Product (GDP) with crops production accounting for 80 %, while livestock and fishery account for 13 % and 4 % respectively [1]. One of the key agricultural crops in Nigeria is palm fruit which is found mostly in Southern Nigeria especially in the wet rain forest savannah belt. It also exists in the wet part of North Central Nigeria in areas such as Southern Kaduna, Kogi, Kwara, Benue, Niger, Plateau, Taraba, Nasarawa, Osun and Ondo States [2]. Solid wastes from palm tree comprise of Empty Fruit Bunches (EFB), Palm Press Fibre (PPF) and Palm Kernel Shell (PKS). These solid wastes from palm tree accounting for 20-23 % of EFB, 12-15 % of PPF and 5-7 % of PKS based on its capacity [3]. However, much of these biomass wastes are left to decay in plantation areas or creating environmental nuisance [4]. Utilizing wastes, particularly PKS from oil palm industry for energy purposes could support the existing energy sector in Nigeria.

There are several technologies that enable oil palm mill to generate enough energy for its consumption and sometimes for export. Among them are fixed (1 kW- 50 MW), fluidized (5 MW- 100 MW) and dust technology (10 MW- 500 MW). Efficiencies of these technologies are dependent on fuel properties and the mixing quality between flue gas and combustion air [5]. Ninduangdee and Kuprianov [6] recorded high combustion efficiency and low emission performance in a fluidized bed combustion of palm kernel shell using optimized particle size, although the start up and running cost of operation associated with this technique make it difficult to be operated by small scale business. Remarkable improvement has also been recorded on design of large scale grate furnaces (fixed bed), yet additional work need to be done in small scale businesses in term of poor mixing especially when co-firing different fuel and high moisture fuel content for improve combustion and reduction of ash deposition on components of grate furnace [7]. The unique features of grate furnace are the tolerance of fuel type; positive movement of fuel down grates reduces blockages and well controlled air distribution lead to high combustion efficiency [8]. These will increase combustion process and decrease ash deposition. Boiler design is a complex and time consuming procedure. Previously, emphasis was laid on primitive and probabilistic design processes which resulted in high cost of production. Dimensions of boiler for power generation often depend on fuel and vaporization efficiency; the mass balance, heat balance and heat

transfer which has to be specified through empirical results and experiences. In this paper we aimed at design and estimate the cost of palm kernel shell combusting furnace for 5 kW power rating.

II MATERIALS AND EQUIPMENT

The basic materials for this study were palm kernel shells and additives (Al_2O_3 , MgO and CaO) obtained from palm oil mill in Ogbomosho and Ilorin respectively. The equipment used include the air flow metre, Spectrophotometer, 12 points temperature channels recorder, air quality metre, X-ray diffractometer, muffle furnace, Gallen Kamp Bomb Calorimeter.

2.1 Furnace Operation and Development of Power Plant Components

The furnace under consideration was based on principle of water tube natural circulation. The main components of this furnace are steam drum, downcomer, riser tubes which represents the complete fluid flow loop. Water flows to the steam drum through downcomer riser loop. The riser tubes were situated inside furnace where heat of flue gases vaporizes the water into steam and back to the steam drum through steam header collection (Fig. 1). Due to the fact that steam water mixture inside riser tubes is less dense than the saturated water at inlet tube, fluid flows upwards in the riser tubes and back to the drum. The density difference between water at the inlet tube and steam-water mixture produces enough force to overcome friction and gravitational resistance to flow, therefore maintain a steam flow system [9]. The steam drum is partitioned into two zones. The lower section allows water intake to the drum while the upper section produces steam which flows from the top of the drum into the superheater tube. The superheated steam is expected to turn turbine to generate electricity

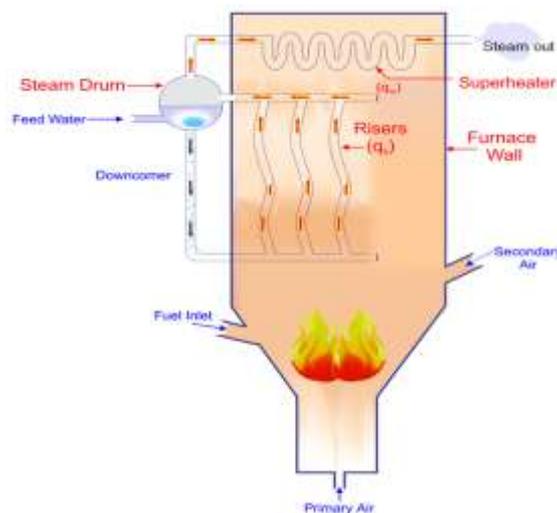


Figure 1. Schematic diagram describing water to Steam Circulation Loop

2.2 Refractory Brick Developed for Lining Furnace

The raw materials used in this study were kaolin, ball clay and hard wood sawdust. The sawdust in the mixture form uniform pores in order to allow heat energy stored in kaolin and it did not bloat while ball clay serves as binding agent. The kaolin was collected from Titibi in Awo, Osun State, Nigeria, while the ball clay and sawdust were collected from Orile – Igbon, Ogbomosho, Oyo State. The ball clay was soaked in water for five days to allow it to dissolve completely in orders to separate colloids from pebbles. The kaolin was milled to powder form using ball mill and then sieved to particle size of diameter 2.5 mm. The ball clay was sieved to 1.0 mm and similarly powders of sawdust of particle size 2.5 mm. The study carried out had a composition of kaolin as 60% by weight while ball clay and sawdust are 30% and 10% respectively according to [10]. The mixture of these powders with water was then rammed into a rectangular specimen with dimensions (275 mm×130 mm×60 mm) as shown in Fig. 2. The samples were sun dried for two weeks and then fired to 1200 °C in a kiln, a Pyrometric Cone Equivalent (PCE) was used to test the refractoriness of the bricks developed. About 80 sample formulations had a total of 300 g (180 g of kaolin, 90 g of clay and 30 g of sawdust).

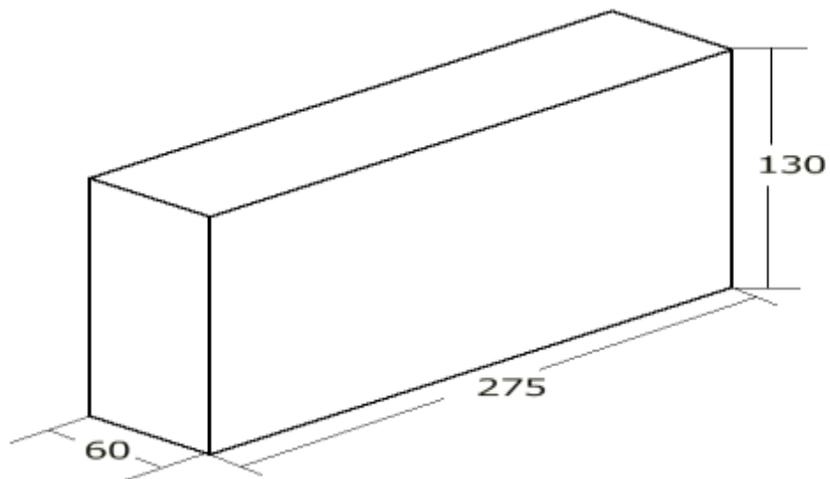
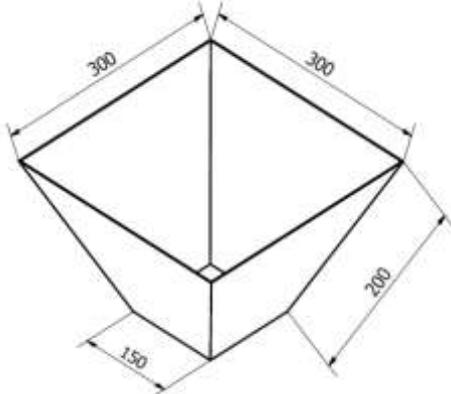
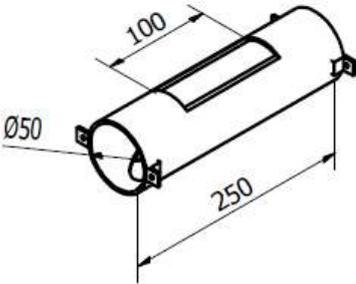
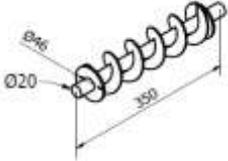
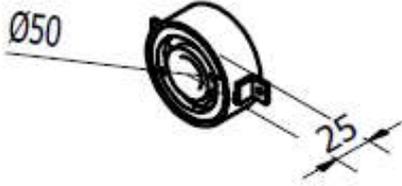


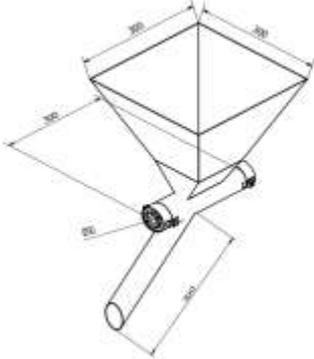
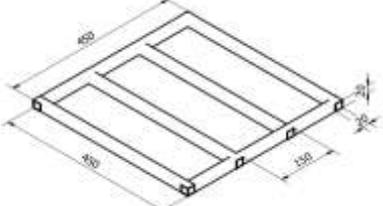
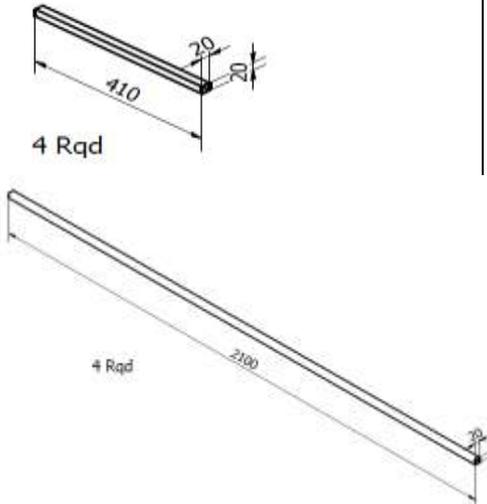
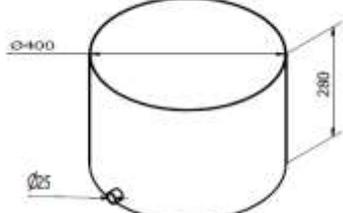
Figure 2. Refractory brick

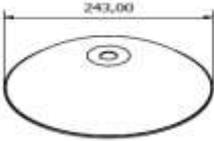
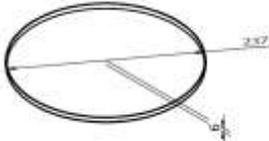
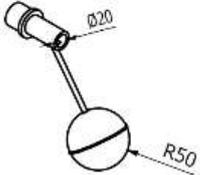
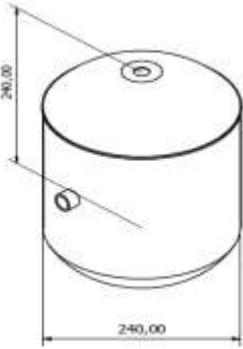
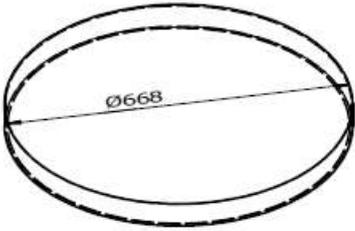
2.3 Fabrication Procedure and Assembly of Developed PKS Furnace

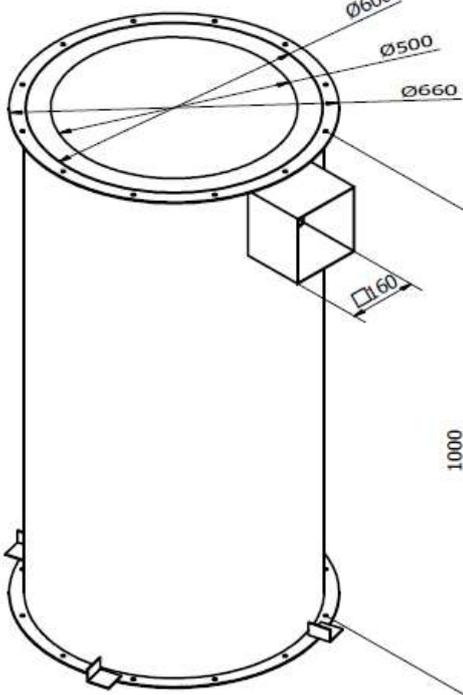
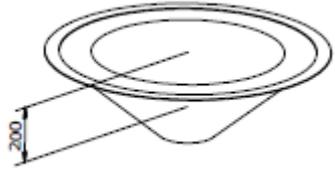
The components of the furnace developed are feeder, riser, water tank, steam drum, and furnace chamber. Each of the component's fabrication process, design and measurement, material selection and cost were shown in Table 1 according to Oladosu et al., (11). Fig. 3 shows the exploded view of the developed PKS combustion unit.

Table 1: Fabrication Processes of PKS Furnace

| Component | Fabrication process | Component design and measurement | Material selection |
|--------------------------|---------------------------------------|--|--|
| Loading hopper | Cutting and welding steel plate |  | Steel plate, chisel, hammer, grinding disk and electrodes. |
| Auger housing | Boring of steel pipe |  | Chisels, ball and pine hammer, drill bits and half round files |
| Auger and screw conveyor | Cutting and welding |  | Chisels, cutting disc, hammer, hacksaw and electrodes |
| Bearing housing | Welding of housing bearing and flange |  | Files, chisels hammer and electrodes |
| Discharged pipe | Drilling and cutting of steel pipe |  | Drill bits, hacksaw, and files |

| | | | |
|--|--|---|---|
| <p>Assembly of hopper, auger housing, bearing and discharge pipe</p> | <p>Assembly of hopper unit using welding machine</p> |  | <p>Electrodes, ball bearings</p> |
| <p>Water tank frame</p> | <p>Cutting and welding of square pipe</p> |  | <p>Vice, hacksaw and electrodes</p> |
| <p>Tank support</p> | <p>Cutting and welding of angle iron to hold up water tank and brazing</p> |  | <p>Vice, hacksaw and electrodes</p> |
| <p>Water tank</p> | <p>Cutting and welding of steel plate</p> |  | <p>Chisel, hammer, anvil, drilling machine and electrodes</p> |

| | | | |
|---|---|--|---|
| <p>Assembly of water tank and frame</p> | |  | <p>Electrodes, try squares</p> |
| <p>Drum cover</p> | <p>Cutting and drilling of steel plate</p> |  | <p>Shear cutting machine, drill bit</p> |
| <p>Steam separator</p> | <p>Cutting of steel plate</p> |  | <p>Spinner, hammer</p> |
| <p>Inlet water pipe control valve</p> | <p>Cutting and external thread of shaft</p> |  | <p>Tap and die, drill bit, and hacksaw</p> |
| <p>Assembly of drum cover, steam water separator and inlet water pipe control valve</p> | <p>Drilling and welding of drum using welding machine</p> |  | <p>Electrodes,</p> |
| <p>Furnace lid</p> | <p>Cutting and welding of flat sheet plate</p> |  | <p>Hand shear cutter, electrodes, chisel and hammer, mild steel</p> |

| | | | |
|----------------|---|---|---|
| Furnace | Cutting and welding, stack up the developed bricks to the wall furnace of |  | Galvanized steel, mixture of kaolin, ball clay, sawdust, and water, |
| Furnace bottom | Cutting and welding of cone shape |  | Mild steel, divider, protractor |

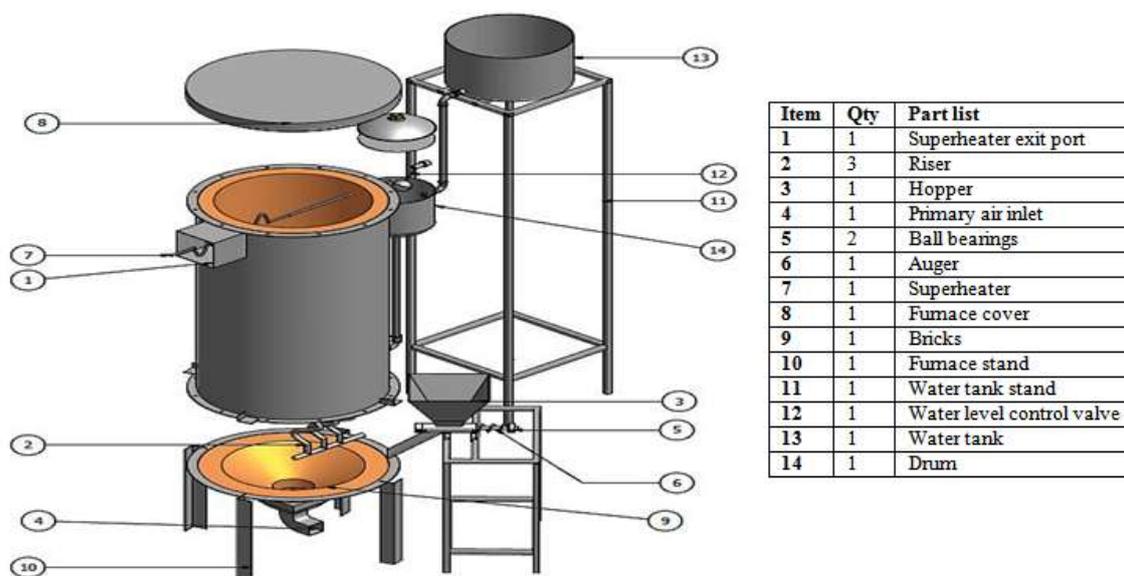


Figure 3. Exploded view of the developed PKS Combusting Furnace Unit

2.4 Experimental set up

The assembly of the furnace (Fig. 4) was designed in two sections: A conical section (0.25 m height with 45° cone angle and 0.2 m inner diameter at the bottom plane) and cylindrical section (of approximately

0.4056 m³ combustion volume and inner diameter of 0.6 m). The two sections had 0.5 m thick metal wall lined internally with refractory brick insulations of 0.25 mm thickness. Feed water was supplied to drum boiler and down comer risers loop connected to superheater tube. In addition, facilities for measurement were such as 12 points channel temperature recorder, air quality meter and air flow meters were used. The primary and secondary air flow was employed in the furnace for ensuring better mixing quality required for good combustion. Five K-type thermocouples with tips along the axis of combustion chamber for temperature measurement and air quality meters to detect CO, CO₂, and O₂, which were placed at different locations in the grate furnace (above the grate, core of the furnace, steam collection header, above steam header and exhaust port). Oladosu et. al., [12] reported the optimum mixture of PKS and selected additives for maximum combustion efficiency as [Al₂O₃ (2.5 %), MgO (0.0 %), CaO (5.0 %), PKS (92.5 %) and particle size (5.50 mm)] and the major operating variable, primary to secondary air ratio were selected for the test. The fuel feed rate was maintained to be constant (3.24 kg for every quarter an hour up to a maximum of 17.3 kg/hr. (in all combustion test).



Figure 4. Fabricated PKS Combusting Furnace

III RESULTS AND DISCUSSION

These are based on: evaluation of the furnace combustion efficiency based on primary to secondary air supply ratio, comparative view of results obtained with state properties of superheated steam generated for 5 kW power rating ease of maintenance, safety and health considerations and economic cost.

3.1 Evaluation of the Furnace Based on Combustion Efficiency when Firing PKS at Different Ratio of Primary to Secondary Air Supply.

Combustion efficiency based on primary (Pry) to secondary (Sec) air ratio, CO, CO₂ and temperature of flue gas were reported (Table 2). It was observed that air split ratio of 40:60 recorded maximum combustion efficiency (64.5%) and it is well comparable with the efficiency of biomass combustor for Agro-industry reported by Rogaume et. al. [8].

Table 2: Summary of test parameters on effect of the primary to secondary air supplied on combustion efficiency and gaseous emission

| Pry: Sec air ratio | Fuel feed rate (kg/hr) | Temperature (°C) | CO (ppm) | CO ₂ (ppm) | $L_{thermal}$ (%) | $L_{chemical}$ (%) | Combustion efficiency (%) |
|--------------------|------------------------|------------------|----------|-----------------------|-------------------|--------------------|---------------------------|
| 30:70 | 17.3 | 760 | 301 | 7484 | 11.00 | 27.76 | 61.24 |
| 40:60 | 17.3 | 785 | 285 | 8497 | 11.03 | 23.49 | 64.58 |
| 50:50 | 17.3 | 673 | 372 | 7006 | 9.60 | 36.69 | 53.71 |
| 60:40 | 17.3 | 620 | 408 | 6875 | 8.71 | 41.01 | 50.28 |

3.2 Comparison of the results obtained with data sheet for steam turbine generator for 5 kW power rating

By way of validating these results, a search was done where PKS was used to generate steam for electricity production and from website V-FLO pump and system (www.V-FLO.COM). Power rated (5–45) kW requires maximum inlet temperature and pressure range of 400 °C and (0.45–4.2) MPa respectively and from this study, 5 kW requires maximum inlet temperature of 200 °C and pressure of 0.38 MPa, (Table 3). Assuming direct proportionality the results obtained is better or probably within the range.

Table3: Differences between the developed and imported 5 kW PKS Steam generator

| Parameters | This study | V-FLO Pump and system www.V-FLO.COM |
|---------------------------------|------------|--|
| Power rated (kW) | 5.00 | 5 – 45 |
| Inlet maximum temperature (°C) | 220 | 400 |
| Pressure (MPa) | 0.38 | 0.45 - 4.2 |
| Mass flow rate (kg/s) | 0.023 | |

3.3 Cost Analysis

The materials and equipment used for the PKS combusting furnace design is shown in Table 4. The materials and equipment used are locally sourced and the overall cost for sizing the furnace component is approximately \$ 1,658.906 (assuming ₦320 exchange rate to 1 dollar). The furnace (steam generator) is cheap in comparison to similar design overseas \$ 2,223.6 (www.ecpush.com). This would greatly be interesting and be useful as energy back up in oil palm mill industry

IV CONCLUSIONS

The research was focus on the design and cost estimate of palm kernel shell combusting furnace for 5 kW power rating. The design philosophy is to alleviate unreliable energy supply in Nigeria which has left the rural dwellers socially backward with untapped economic potential. On completion and testing of the developed furnace it was observed that the primary to secondary air supply of (40:60) recorded highest combustion efficiency of 64.5% for a fuel feed rate of 17.3 kg/hr. The maximum steam temperature, pressure and mass flow rate recorded for 5 kW power rating were 220 °C, 0.38 MPa and 0.023 kg/s respectively. The overall cost for sizing the furnace component is approximately \$ 873,857 assume N 320 exchange rate to 1 dollar. The furnace (steam generator) is cheap in comparison to similar design overseas \$ 1350.6 (www.ecpush.com). This would greatly be interesting and be useful as an alternative source of energy

Table 4: Bill for Engineering Measurement and Evaluation

| Materials | Specification | Quantity | Cost (₦) |
|---------------------------------|------------------|------------|----------|
| 1 mm steel sheet | Mild steel | 3 sheets | 16,000 |
| 1mm stainless sheet | Stainless | ¼ sheet | 8,000 |
| Ø 50 mm × 1.2 mm steel pipe | Mild steel | Length | 2, 500 |
| 25mm× 25mm × 3mm angle iron | Mild steel | 3 lengths | 4,500 |
| 25 mm× 25 mm ² pipe | Mild 35steel | 2 lengths | 1,450 |
| Ball bearings | Stainless | 2 numbers | 2,500 |
| Ø 25 mm × 2 mm pipe | Stainless | 3 lengths | 12,000 |
| Ø 25 mm × 1.6mm pipe | Stainless | ½ length | 4,000 |
| Ø 500 mm × 1700 mm × 4 mm | Galvanised steel | 1 | 18,000 |
| Ø 40 mm × 600 mm shaft | Mild steel | 1 | 1,900 |
| 15W reversible motor | 1 | 1 | 4,500 |
| Centrifugal blower 1horse power | 1 | | 5,500 |
| Electrode | Stainless | 1 dozen | 1,500 |
| Electrode | Mild steel | 2 packets | 4,500 |
| Ball clay, kaolin and sawdust | | Lot | 8,500 |
| Mold making | | 92 samples | 3,500 |
| Gas for firing bricks developed | | 20kg | 14,000 |

| | | | |
|---|--|---|-----------|
| 6 points channel temperature recorder | | 1 | 33,500 |
| Thermocouple | | 4 | 26,500 |
| Transportation | | | 45,500 |
| Gas flow metre, gate valve and plumbing | | | 55,000 |
| Labour | | | 75,000 |
| Overhead cost | | | 15,000 |
| Turbine (5.5 kW)) | | 1 | 125,000 |
| Total | | | ₦ 488,350 |

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